

ASL-TR-0029



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EFFECTS OF ARRIVAL TIME ERRORS IN WEIGHTED RANGE EQUATION SOLUTIONS FOR LINEAR BASE SOUND RANGING

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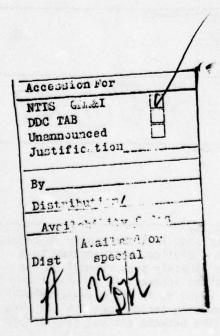
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20. ABSTRACT (cont)

at one or more microphones is shown to be approximately linear and to possess the property of superposability; i.e., the combined effect of several errors in arrival time is approximately equal to the sum of the effects of each error taken as occurring alone. Several general properties of symmetry and antisymmetry are demonstrated.

This report provides its readers with the basic vector error response of the Weighted Range Equation Solution for all areas in which the AN/TNS-10 Sound Ranging Set is effective.



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INTRODUCTION

Linear base sound ranging, using the GR-8 or AN/TNS-10 Sound Ranging Set, has been shown to be an effective means for locating enemy firing batteries which are beyond the range of direct visual observation. Development of the USRAN3 solution technique by Swingle, Bellucci, and Crenshaw showed that the present system was not performing to the limits of its accuracy potential. Their evaluations showed that an improvement in accuracy from 2.2 percent of range* to 1.8 percent could be achieved by a simple change in the method by which the final target location (fix) was computed. 1,2 They noted that further improvements were believed to be achievable.

In response to a request from US Army Materiel Command Headquarters in June 1974, Swingle developed an error analysis for the overall system which was used to estimate the likely improvement which could be achieved for a typical target located centrally to the microphone array and 10,000 meters ahead thereof. This restriction of target location was adopted for reasons of both simplicity and nonavailability of quantitative error sensitivity data for other locations.

The present report covers the first steps in expanding that analysis to include the entire field of potential target locations, including extension of the analysis to points beyond the usual range of sound ranging utility, i.e., to ranges exceeding twice the base length and to flanking angles beyond 15 degrees from the normal of the outlying subbases.

This analysis will develop the ultimate accuracy which can be expected from a variety of sound ranging array configurations having tactical practicality, including, of course, the six-microphone "linear base" system with which the US Army is now equipped. Optimized meteorological correction methods, which take account of the natural variability of the atmosphere, will be considered as parts of the overall sound ranging system input error source.

It will be assumed that the reader is generally acquainted with the principles of sound ranging on artillery weapons based on the use of the AN/TNS-10 or similar system. All six microphones will be assumed to be installed along a straight base at uniform spacings of four sound seconds (about 1350 meters). While solutions for shot time and shot coordinates are unique, within the usual assumptions of an atmosphere having uniform

^{*}Distance target is forward of line of microphones

¹Donald M. Swingle, Craig M. Crenshaw, and Raymond Bellucci, 1972, "Improved Sound Ranging Location of Enemy Artillery," Army Science Conference, US Military Academy, West Point, NJ

²Donald M. Swingle and Raymond Bellucci, 1973, "Improved Sound Ranging Location of Enemy Artillery," R&D Technical Report ECOM-5486, US Army Electronics Command, Fort Monmouth, NJ

wind and uniform temperature (sound speed), when arrival times from only three microphones are used to determine target location, the system is over-determined when more than three arrival times are used. Under these conditions a number of solution methods can be used, yielding generally different target locations.

Following the development and evaluation of the USRAN3 solution, Crenshaw and Swingle engaged in a continuing verbal and correspondence exchange, 3,4 looking forward to a more general and even more accurate solution and meteorological correction method. This led to the evolution of the Weighted Range Equation Solution (WRAS) which is outlined in the appendix. In brief, this method determines the shot time and coordinates which minimize the sum of the squares of the differences between the square of the geometric range from solution point to each microphone and the square of the "propagation range" computed from the speed of sound along that direction and the difference between computed shot time and measured arrival time.

$$\sum_{i=1}^{N} W_i \times \left(R_i^2 - P_i^2\right)^2 = minimum \tag{1}$$

where W_i is a weighting factor which may be varied by any desired rule across the microphone array. A simple form for the W_i which was suggested by the known behavior of atmospheric variability as studied by Arnold and Bellucci⁵ and later by Lowenthal and Bellucci⁶ is

$$W_{i} = R_{i}^{n} / \sum_{i=1}^{N} R_{i}^{n}$$
 (2)

³Personal communications between Dr. Craig M. Crenshaw and Dr. Donald M. Swingle, June 1972-December 1973

⁴Craig M. Crenshaw, 1972, "Sound Ranging Calculations," AMC Chief Scientist Technical Note Number 1, US Army Materiel Command, Alexandria, VA

⁵A. Arnold and R. Bellucci, 1957, "Variability of Ballistic Meteorological Purameters," Technical Memorandum M-1913, US Army Signal Engineering Laboratories, Fort Monmouth, NJ

⁶Marvin J. Lowenthal and Raymond Bellucci, 1970, "Variability of Ballistic Winds, R&D Technical Report ECOM-3259, US Army Electronics Command, Fort Monmouth, NJ

where n is any real number. Experimentation was conducted with n ranging from 0 to -10. When applied to actual sound ranging data, n = -5 generally gave the most accurate target locations. In the present study this weighting was used, but the conclusions are equally valid when solutions are computed using n = 0.

Earlier studies of sound ranging system error sensitivity had been conducted by Fox, Lee, 8 and Bellucci. 9,10

All the above utilized solutions depended upon use of <u>differences</u> in arrival time at adjacent microphones. Fox used a least squares minimization of the differences between "true" and perturbed arrival time differences, while Lee minimized the squared differences between "true" and perturbed arrival times. Bellucci used the standard artillery solution. Bellucci's published work was confined to a set of only 12 points in the target area. Lee expressed errors as radial errors (i.e., miss-distance), thus precluding consideration of the vector nature of the error patterns. Fox considered radial and tangential errors relative to the center of the microphone array. Lee presented total radial error contours but provided no data on vector error. None of the researchers provided a dense, ordered array of errors at target points throughout the battle area which might be utilized for error analysis of both current and future tactical sound ranging systems.

Results obtained herein are in generally good agreement with these studies. They differ in that they present error transfer properties of the WRAS solution in terms of along-array and along-normal components. They also extend the range of the computations to at least five sound base (25 subbase) lengths ahead of the array and to 9 to 18 subbase lengths to either side of the centerline of the array. Additional computations, not covered in detail here, extend the computations out as far as 15 sound base (75 subbase) lengths forward of the array. The properties of linearity and superposability discussed below were also found to extend to such ranges, although

⁷H. L. Fox, 1968, "Meteorological Techniques for Sound Ranging; Theory of Errors," Technical Report ECOM-0233-2, US Army Electronics Command, Fort Monmouth, NJ

⁸Robert P. Lee, 1972, "Artillery Sound Ranging Computer Simulations," R&D Technical Report ECOM-5441, US Army Electronics Command, White Sands Missile Range, NM

⁹Raymond Bellucci, 1966, "Studies of Meteorological Techniques for Sound Ranging: Report II, Error Analysis," Technical Report ECOM-2703, US Army Electronics Command, Fort Monmouth, NJ

¹⁰Personal communications between Raymond Bellucci and Dr. Donald M. Swingle, June 1966-June 1972

errors were generally much larger. These results will be utilized in succeeding reports dealing with errors in microphone position and atmospheric input as well as terrain effects and sound ranging system improvement.

DATA PRESENTATION

The data of this report are uniformly presented as fields of numerical values, to provide, in a reasonably compact form, the detailed information required to assess the effects of various error sources on target location. Those readers whose taste leads to the representation of data in contour maps are invited to add their own analyses of the numerical fields presented. Both horizontal components of target location error are presented at each grid point to facilitate ready analysis of the vector character of the target location error associated with input data errors.

DATA INTERPRETATION

Figure 1 provides a schematic guide to interpretation of the following tables. Tables 1 through 23 provide the field of target location errors due to specified errors in arrival time at given microphones for each of a regular array of assumed "true" target locations. The targets are assumed to be at the points indicated by "+" (except along the left-hand edge of the figure).

These points are uniformly spaced by one subbase length forward of the center of each subbase and laterally from the center of the array. To the left of each target point appear two figures. The upper number is the error in meters which would arise in the solution by WRAS for the target along the X- or along baseline direction, while the lower number is the error in the Y- or normal-to-baseline direction.

Along the top of each figure are listed the subbase length (BL) in sound seconds (4 sound seconds is approximately 1350 meters) and the index number of the perturbed microphone (IP, counting from left to right as one faces the target from the baseline). In this report IP will range from 1 to 6. If two digits are given under IP, these digits indicate the two microphones whose arrival times are simultaneously perturbed. ID is used to indicate the perturbed parameter and will always be 8 in this report, indicating that the perturbation considered is in time of arrival at the microphones indicated by IP. The number of subbase lengths to the right of the array center which characterizes the top row of targets (+) is given by M. As the computations progress down the page, M is incremented for each row and appears at the left-hand edge of the paper abreast of the Y-component of error. Just above these changing values of M appears the value of IP given in the heading line. This value appears just to the left of the first + in each row which marks the point which is M subbase lengths from the array center. In all of the tables N = 25, indicating that the right-most + or target position in each row is 25 subbase lengths

forward of the microphone array. DXY indicates the spacing in both X and Y directions of the grid points in units one subbase long. In all tables herein DXY is 1.000. UP gives the assumed unit perturbation which is applied to the arrival time of the identified microphone(s) expressed in milliseconds. IW is the weighting exponent. In terms of equation (2), n = -IW. IW will always be 5 herein. ZZ gives the target height above the plane containing the microphones and is always 0.0 in this report. V1, V2, and V3 are the X-, Y-, and Z- components of the mean wind assumed in the computation, and will remain 0.00 in this report. Finally, TE is the assumed "effective temperature" for sound ranging, assumed to be 10° C herein.

Where **** appears on the tables, the error exceeds ± 999.5 meters, while $^{-0+}_{-0}$ appearing in the upper and lower left corners indicates that computations were not made for the point because it occurs at a large flanking angle (|M| > N + 3).

EFFECT OF UNIT INPUT ERRORS ON SOLUTIONS

In computing the data for tables 1 through 15, the author assumed that the target was at the plotted grid point, and the arrival time of sound generated at shot time (= 0.000 seconds) was computed for each microphone. Then the arrival time at the specified microphone (IP) was incremented by UP milliseconds, and the target location was computed by using the WRAS solution. At the field point the difference between the computed location and the assumed or "true" location is printed (computed - true). In tables 1 through 6 of "error maps," the unit perturbation was assumed to be 1 millisecond. All errors are rounded to the nearest meter. This value was chosen as small enough to produce few errors exceeding 1000 meters, while also producing few errors less than a few meters in at least one of the component directions. The reader is invited to examine the symmetry of error effects between microphones 1 and 6 (tables 1 and 6), 2 and 5 (tables 2 and 5) and 3 and 4 (tables 3 and 4).

The tables show that errors in arrival time at microphones 2 and 5 have relatively small effects at most target points on either component of target location error and that for all microphones the Y-component error is generally several times the X-component error. Further, both microphones 1 and 6 yield large negative Y-component errors for a small positive change in arrival time, while both microphones 3 and 4 yield large positive errors in Y-component for a small positive change in arrival time.

In the above computations and throughout this report, it does not matter whether the "error" in arrival time be the result of an error in reading the acoustic record or the effect of propagation phenomena in causing the signature's apparent arrival time to be different from that which would be expected after correcting for the assumed meteorological conditions. Either cause will result in the same target location error if it

causes the same error in arrival time. For example, at the point M = -9, N = 25, the upper right-hand + in table 1, one finds that an arrival time error of 1 millisecond (UP = 1.00) causes the X-component of target position to be computed to be 18 meters larger than true and the Y-component to be computed to be 49 meters smaller than true (18, -49). For the same point, tables 2 through 6 show that the same unit error, if it occurs at microphones 2 through 6, produces target location errors of (-5, 17), (-14, 40), (-11, 31), (-1, 1), and (13, -41) meters, respectively.

LINEARITY OF ERROR TRANSFER FUNCTIONS

The analysis of the joint effects of several error sources on the overall sound ranging target location error would be much simplified if the output error could be assumed to be linearly dependent upon the input error, or at least approximately so. Tables 2 through 6 show the error fields for input errors of 1 millisecond occurring in microphones 1 through 6, while tables 7 through 12 show the error fields for input errors of 3 milliseconds.

In view of the symmetry noted for errors in microphones 1 and 6, 2 and 5, and 3 and 4, it becomes apparent that the entire story can be told by just the error fields due to microphones 1, 2, and 3. Thus the error fields due to input errors of 10 and 30 milliseconds, shown in tables 13 through 15 and 16 through 18, respectively, are shown only for microphones 1, 2, and 3.

Through most of the error field, output errors in each horizontal component of target location are approximately proportional to input errors. Over a range of 30:1 in input error, proportionality is quite good. The range selected for illustration includes the range of errors to be expected because of normal atmospheric propagation effects and from errors in reading arrival time records.

In assessing the combined effects of several errors affecting the measured arrival time at any microphone, little error will occur if the target location error due to each contributing error is separately computed and the results summed instead of first summing the several contributing errors in arrival time and then computing the target location error which they will cause.

SUPERPOSABILITY OF ERROR TRANSFER FUNCTIONS

The preceding section demonstrated that several simultaneous arrival time errors occurring at a <u>single</u> microphone could be separately transformed into target location errors and then summed to give the aggregate target location error. To investigate the validity of computing errors due to simultaneous arrival time errors in <u>several</u> microphones as the sum of the effects of errors in each microphone, the author assumed errors occurring in one microphone and an additional error occurring in each of the remaining microphones in turn.

In tables 19 through 23, simultaneous errors of 3 milliseconds are assumed to occur in microphone 2 and in microphones 1, 3, 4, 5, and 6 in turn. The reader will be able to readily verify that the effect of the combined simultaneously occurring error is very closely approximated by the sum of the errors given table 8 and tables 7, 9, 10, 11, and 12, respectively.

For example, tables 7 through 12 show that the errors in target location at the point (M, N) = (-9, 25) due to a 3-millisecond error in arrival time at microphones 1 through 6 are (56, -147), (-15, 50), (-42, 120), (-34, 93), (-3, 2), and (40, -124) meters, respectively. For the same target point, table 19 shows that the target location error due to simultaneously occurring 3-millisecond errors in microphones 1 and 2 is (40, -95), almost exactly the sum of the effects of this error acting separately at microphones 1 and 2. The corresponding effect of the combined error in microphones 2 and 3, 2 and 4, 2 and 5, and 2 and 6 are (-58, 172), (-50, 145), (-19, 53) and (15, -74) meters, respectively, as shown in tables 20 through 23. In each case the effect of the simultaneously occurring error is approximately equal to the sum of the effects caused by each error taken as acting alone. Similar results would be found for any selected group of microphones and for any target point.

We have thus shown that the errors in target location resulting from the simultaneous presence of errors in several microphones can be closely approximated by the sum of errors computed as if each error occurred separately in each of the microphones.

CONCLUSIONS

The above analysis has shown that sound ranging solutions obtained by the WRAS solution technique applied to a regular, linear, six-microphone array have the following properties:

- 1. Errors occurring in arrival time, relative to the assumptions inherent in the solution model, in microphones 1, 3, 4, and 6 have the greatest effect on the solution; while at most field points, microphones 2 and 5 have relatively little effect on the solution.
- 2. At most field points, the Y-component of target location error due to an error in arrival time at any microphone is generally several times as large as the X-component of error.
- 3. Positive errors in arrival time at microphones 1 and 6 lead generally to negative Y-component errors, while positive errors in arrival time at microphones 3 and 4 result in positive Y-component errors.
- 4. Positive errors in arrival time at microphones 1 and 6 lead to positive X-component errors in target locations for left flank targets and negative X-component errors in target locations for right flank targets, while positive errors in arrival time at microphones 3 and 4 lead to positive X-component errors in target location for right flank targets and negative X-component errors in target location for left flank targets.

- 5. For each horizontal component of target location, the error caused by an error in arrival time at any microphone is approximately proportional to the arrival time error; i.e., the time-to-space error transfer function is approximately linear. Thus the error in target location due to the combined effects of several errors in arrival time at any one microphone is closely approximated by the sum of errors in target location which each of the contributing errors would have caused if acting alone.
- 6. The error in target location in each component of position resulting from simultaneously occurring errors at two or more microphones is closely approximated by the sum of the errors which each arrival time error would produce if acting alone; i.e., the error contributions are superposable in geometric space.

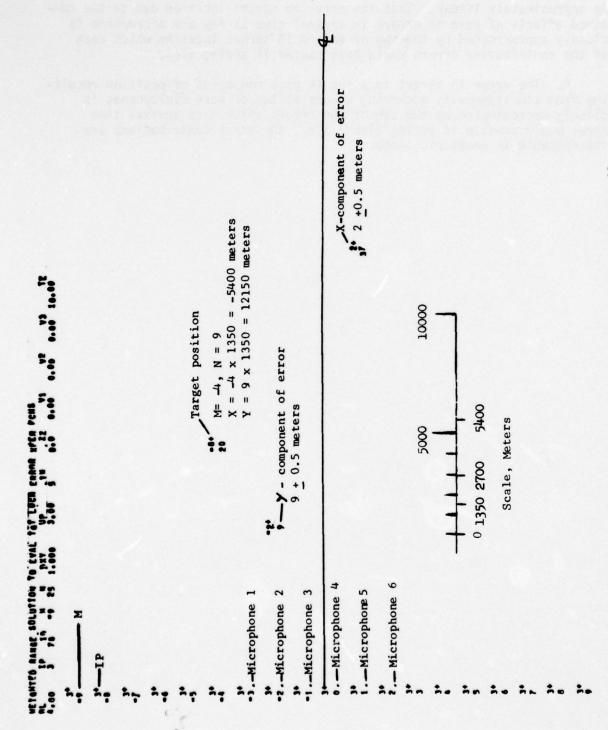


Figure 1. Key to error maps, tables 1 through 23.

TABLE 1. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

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TABLE 2. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

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TABLE 3. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

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	22	12	÷ •	:=	:=	÷=	÷=	÷=	\$=	52	\$ 2	-~	-=	==	÷=	:=	÷ 2	÷~	2 2
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TABLE 4. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 4

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	:2	tz	÷2	*2	* 2	:2	:2	*2	÷2	6 %	50	*~	* 2	: 2	• 2	* =	- 2	==	22
	:=	÷s	fa	*:	÷۵	: 2	÷ 2	:2	÷s	\$2	52	22	* 2	: 2	:	22	:0	==	===
	† 2	+=	*=	* =	÷ 2	÷ 2	. 2	*=	÷=	• 2	\$ 2	- 22	. 5	- 2	* 2	2 %	= 2	20	22
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2.	••	••	**	• • •	==	*:	:.	••	:.	:.	••	••	÷ ~	÷:	• • •	::	• •	**	••
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TABLE 5. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 5

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TABLE 6. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 6

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	-:	**	= 2	-22-	\$ 92	-50	-50	-50	-50	-50	-22	-22	. 50	.500	• =	-10+	-34	***	
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						.51												::	::
	-53	-52	- 2	-50	*:	÷ 61.	.161.	-67	50	60.	-50	. 20	÷ =	.52	÷ ?	\$ 52.	-111-	-13+	• =
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						.12												-13+	-10
20		::	:5	::	* :	-10 -11 -13	-:		35	• =	77		::	÷:		••	-104	-13	- 52
	::	-:	÷ =	: 2	* 2	*=	==	• =	•=	•=	: 57	-13	*	:5:		::	56	-213	-23
	• :	\$ 27	÷ =	::	.01	. 0 .	-:	50	• • •	00		::-	.15	::		÷ •	00-	-13+	- 25
2000	: .	:=	: 0	= 0	* *	*:		::	:	÷ •	- 0			1:	4:	1:	- 4		
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X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE TABLE 7.

HETGHTED RANGE SOLUTION TO EVAL TAT LOCK ERROR MFER PCNS

-93 -102 -110 -119 -95 -103 -112 110 120 120 36* 37* 36* 39* 40* 41* 20+ 21+ 22--97 -105 -113 -122 *13 *13 *14 *51+ *22+ *13* -30+ -31+ -33+ -34+ .17. -18. -18. -23+ -26+ -27+ -28+ -93 -100 -107 -115 -123 -132 -140 25+ 26+ 26+ 27+ 28+ -99 -107 -116 -96 -104 -113 .04 -103 -112 -94 -103 -112 -95 -103 -112 -96 -105 -113 -98 -106 -115 -92 -100 -109 -118 • +94 : 11. . -01 .. - 60 -98 10+ 60. -13+ - 83 •3• * 0 -10 .72 ÷ -. *224 ; .69 19. -14-*= 13+ .514 •20 . . .62 9. .50 19. -01 £ 5. .0. • 10--31 -53 -76 -01 - 25 35. -50 : 324 181 -28 69. 01 04. . 0.00 10,00 ÷. if .53 ÷ -10+ .0. -35 -37 : i: -30 09-04-• 31 .32 35. -11. -24+ .63 -26 -52 -28 -13 200 .51 -22 ... : - 0° 200 -13 . 25. .36 .. -20 .. -25 - 35 .33 .15. : ---13 .. -13 : ---13 91. -101-== -13+ 20--28-7: -10 : .10. .13 13 = •18 -69-*: .33

TABLE 8. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

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		**	+=	*=	::	3.5	÷=	• =	-=	==	22	÷ º		÷.	*•	÷ ~	÷ -	20	-~
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TANGE .	-368	-380	-236	132	**	25	120	-	ă -	• -	• •	• •		† r	*:		??	-62	-106-
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TABLE 9. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

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	8	*=	1.5	2:	==	-:		1:	*:	:	**	22	25	22	= 2	2.2	22	22	102
		35				45	11	1:	2.5	÷ =	*	::	-:	2:	1:	::	102	1.5	130
	36					22	+=	*:	*:	:5	*:	\$ 25	: 2	÷23	13.	19	\$ 53 e	::	56
		2.5	78			- 25	* 5				**	: .		***	: 0	5.4	\$20		.00
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		•			•	- 25							: 5						52
	-				.15.		::						::	* 6	39	::		\$50	43.
			234 -	•										38	==	* 55	3.5	36	38.
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TABLE 10. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 4

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	\$ 2	126	100	::	::	20	*:	::	••	:=	**	::	==	22	::	\$25	200	żr	
	•56	.53	·21.	-10	. 29	15	÷ %	\$ %	::	• \$	**	* 5	==	22		35	2.5	***	::
	. 27.	35	37		= 0	32.5			3.3		*0	\$ 2	:5	12.	40	::	22	22	
	- 56	52.		30	200	500	: 0	*-	÷.2	30	325	**	÷ 5	***	• • •	* ° °	\$22	**	33
		-51	• •	5.5	20	95	• •	• •	÷:	÷ •	**	* =	• 5	÷ 2	2 6	500	\$ 5	\$2	76.
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F 8	33	35	==	30	30		300	:=	32	•	-	: 4	28	500	::	::	23+	23	33
.01	-19+	27	-13	:52	3 5	26	\$ 92	: 2	\$ 55	6 8	-=	::	:5	25		==	22.	22	33.
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TABLE 11. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 5

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TABLE 12. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 6

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	36- 37- 38- 40-	95 -103 -111 -120	25+ 26+ 27+ 28-	-96 -106 -115	17. 18. 18. -06 -105 -113	13+ 13+ 14+ -05 -103 -112	-94 -103 -112	-94 -103 -112	-95 -103 -112	-34 -34 -34	-7+ -7+ -8+ -89 -97 -105 -114	-114 -114 -124 -124 -91 -99 -107 -116	-15161717.	-20+ -21+ -22+ -23+	-25+ -26+ -26+ -27+ -28+ -93 -100 -108 -117 -126	-30* -31* -32* -33* -34* -97 -105 -113 -121 -130	102 -110 -118 -126 -135	135	. 35
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	-63	-59		-54	-53	-52.	• 5	-51	• • • •	-55	-54	.00	-12		-214	-27.	-33+	• • •	- 84
	-57	-53	-51	15.	==	• • •	-39 -45	**	• • •	-35 -41 -46	-37 -42 -48	-39 -44 -50	•12+	•16•	-20+	- 50.	.32.	-13	-48+ -48+
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TABLE 13. X- AND Y-COMPONENT ERRORS DUE TO A 10 MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

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TABLE 14. X- AND Y-COMPONENT ERRORS DUE TO A 10-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

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X- AND Y-COMPONENT ERRORS DUE TO A 10-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3 TABLE 15.

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TABLE 16. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

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TABLE 17. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

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÷ _e	363	316	107.	: 5				102	:5	::	20.	<u>:</u> .	==	::		12	-53		-55.
10.00	346	328	277		101	. 0 .	121	••	• •	÷ 2	::	÷ ?	\$ 22	÷ ;			• • •	:	
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5	:		:		*		::	:	: ;	;	- ;	::			::	::			
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TABLE 18. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

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		322				20	100		-25.	. 2		:0	: 5	127.	150.		721+	711	722
			1634	920	180	129	731	.36.	* 664	:50	36.	***		1224	151+	180.	*11.	651	278.
		300	234.	761	730	701	35	33:	-23.	::		505		114.	37.	177.	584	233.	266.
		100	2510	709	100- 176	121.					::					163.	1914	521+	553+
			•			33.										155.			
					150+			::									171.		228.
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	•		- 0 - 0			•										127.			
¥0	•		505													116.			
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>0				387	154		307	38.		: 150	37.	38.	::	507	\$20	200		133+	
>0.0			30.5	- 1												162			
		366	3.6	1604-	1200			210		*5		31+	::	53+	129	: 5.	• • •	- 2 - 2	120
. 00.0			310	14500	•		-55.		73	**	: 0	20	= =			::	- 0		
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30.00	43	200									: :	::	• •		:	::			
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WEIGHTED RANGE SOLUTION NAME OF 15 A C 25 A					3. 489		*;	*,	*-	*•	÷-	**	**	*-	**				

2 AND X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 1 TABLE 19.

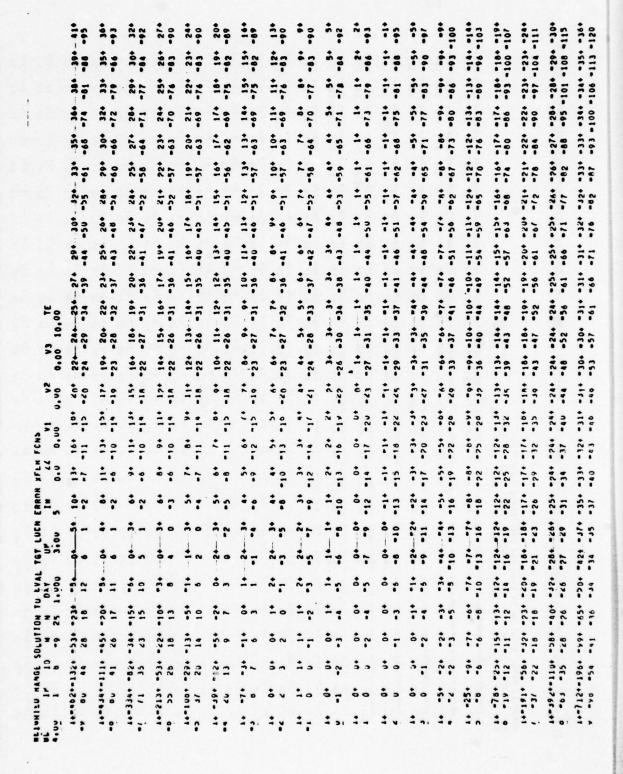


TABLE 20. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 3

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104 112 :01 . . 12 19 At 12 42 42 42 i 121 : : : : : : : : : : :: -11. == 12 :: :: 13 : 124 :: -23+ -11. :: -: :: 105 : 901 100 :: 12 3 5 50 : 2 : :: 10 -62. -60. -58. 96 100 104 : 0.00 10.00 -40. -47. -: 0.00 0.00 -73. -60. -64. A7 90 92 RETURNED MANGE SOLUTION TO LVAL TOT LUCH ERROR XFLM FCNS . . 33 9 .. : 200 -13 33 -9 25 1.v0u -0 405 127 93 79 73 .13 35 5 = -514 -1302-. 34. 34-W36--649--130+ .15 07. 5 87 2. :: .31. *********** 200 -34-11/1-1/6. Š 34-164 163 :: 77. .107 ... ;

TABLE 21. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 4

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TABLE 22. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 5

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APPENDIX

THE WEIGHTED RANGE EQUATION SOLUTION

Given microphone positions $(x, y, z)_i$, arrival time t_i , target position (X, Y, Z), shot time T, effective mean air velocity componets $(u, v, w)_i$ and sound speed c_i , we can write the equation connecting these as follows:

$$\left[\left(X - x_{i} \right) + u_{i} \left(t_{i} - T \right) \right]^{2} + \left[\left(Y - y_{i} \right) + v_{i} \left(t_{i} - T \right) \right]^{2}$$

$$+ \left[\left(Z - z_{i} \right) + w_{i} \left(t_{i} - T \right) \right]^{2} - c_{i}^{2} \left(t_{i} - T \right)^{2} = e_{i} . \tag{A1}$$

With real data, there may be errors in our determination of any of the subscripted variables in the left-hand member, so that the e are generally nonzero. Expansion and rearrangement yield

$$R_i^2 - P_i^2 = e_i$$
, (A2)

where, denoting the effective speed of sound travel toward each microphone by $\mathbf{s_i}$,

$$R_{i}^{2} = (X - x_{i})^{2} + (Y - y_{i})^{2} + (Z - z_{i})^{2}$$
, (A3)

$$P_i^2 = s_i^2 (t_i - T)^2$$
, (A4)

$$s_{i}^{2} = (c_{i}^{2} - u_{i}^{2} - v_{i}^{2} - w_{i}^{2}) - [2/(t_{i} - T)]$$

$$x \left[u_{i}(X - x_{i}) + v_{i}(Y - y_{i}) + w_{i}(Z - z_{i})\right]. \tag{A5}$$

Thus defined, the weighted range equation solution seeks those values of the unknown target coordinates and shot time (X, Y, Z, T) for which

$$\sum_{i=1}^{N} W_i e_i^2 = minimum . \tag{A6}$$

For the purposes of this study, y_i , z_i , u_i , v_i , w_i , and Z are taken to be zero, all c_i are assumed equal to a single value (the speed of sound at an effective temperature of 10°C), and $x_{i+1}^{-x_i}$ is assumed to be a constant, 1350 meters. Based on prior experimentation with real sound ranging data to determine the best exponent n, W_i is defined as follows:

$$W_{i} = R_{i}^{n} / \sum_{i=1}^{N} R_{i}^{n} , \qquad (A7)$$

$$n = -5 (A8)$$

The solution to (A6) is obtained by an iterative computation, using conventional least squares methods and treating the W_i as constants during each approximation.

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